## Interpolation of POD-ROMs for turbo-machinery by grassmannian kriging

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## Context : French Research Agency project HECO



From HEating to COoling
The project : FE simulation of full scale industrial furnace/quenching tank for the prediction of thermal history of formed metal parts.
One problem : Simulation of the axial fans/agitators yields very fine mesh $\Rightarrow$ costly operation
But we are not interested in the high fidelity description of the flow around the rotating solids
Solution replace them by reduced order models


## Objective and approach

## Objective

Build adaptive POD-ROM for a rigid bodies in forced rotation inside a fluid domain.

## Difficulties with POD

1. moving boundaries : not compatible with spatial POD basis.
2. robustness w.r.t change of
 parameters.

## Approach

1. Monolithic description of FSI and exploit the geometry ${ }^{1}$.
2. Interpolation of POD-bases by novel grassmannian kriging ${ }^{2}$.
[^0]
## Multiphase MOR : Domains

## Domains description

- Computational domain $\Omega=\Omega_{\mathrm{S}}(t) \cup \Omega_{\mathrm{F}}(t)$.
- Characteristic function $\chi_{\mathrm{S}}(\boldsymbol{x}, t)= \begin{cases}1 & \text { if } \boldsymbol{x} \in \Omega_{\mathrm{S}}(t) \\ 0 & \text { otherwise. }\end{cases}$


## Rotation velocity

$$
\boldsymbol{u}_{\boldsymbol{\omega}}(\boldsymbol{x}, t)=\boldsymbol{\omega} \times\left(\boldsymbol{x}-\boldsymbol{x}_{\omega}\right), \quad \forall \boldsymbol{x} \in \Omega \text { and } \forall t \in \mathrm{~T}
$$

## Rotation constraint

$$
\begin{equation*}
\boldsymbol{u}(\boldsymbol{x}, t)-\boldsymbol{u}_{\omega}(\boldsymbol{x}, t)=\mathbf{0}, \quad \forall \boldsymbol{x} \in \Omega_{\mathrm{S}}(t) \quad \text { and } \quad \forall t \in \mathrm{~T}, \tag{1}
\end{equation*}
$$

Consequence : no deformation of the solid domain

$$
\begin{equation*}
\mathrm{D}\left(\boldsymbol{u}_{\mathrm{S}}\right)=\nabla \cdot \boldsymbol{u}_{\mathrm{S}}=0, \quad \forall \boldsymbol{x} \in \Omega_{\mathrm{S}}(t), \forall t \in \mathrm{~T} \tag{2}
\end{equation*}
$$

## Multiphase MOR : Governing equations

Navier-Stokes + solid rotation constraint

$$
\left\{\begin{aligned}
\rho\left(\frac{\partial \boldsymbol{u}}{\partial t}+\nabla \boldsymbol{u} \cdot \boldsymbol{u}\right) & =\nabla \cdot \boldsymbol{\sigma}+\boldsymbol{f}-\boldsymbol{\lambda} \\
\nabla \cdot \boldsymbol{u} & =0 \\
\chi_{\mathrm{S}}\left(\boldsymbol{u}-\boldsymbol{u}_{\omega}\right) & =0
\end{aligned}\right.
$$

$\boldsymbol{\lambda}$ is the Lagrange multiplier associated with the rotation constraint.
Boundary conditions

$$
\left\{\begin{array}{lllc}
\boldsymbol{u}_{\mathrm{F}}=\boldsymbol{u}_{\mathrm{D}} & \forall \boldsymbol{x} \in \Gamma_{\mathrm{D}}, & \forall t \in \mathrm{~T}, \quad \text { constant Dirichlet, } \\
\boldsymbol{\sigma}_{\mathrm{F}} \cdot \boldsymbol{n}=0 & \forall \boldsymbol{x} \in \Gamma_{\mathrm{N}}=\Gamma \backslash \Gamma_{\mathrm{D}}, & \forall t \in \mathrm{~T}, & \text { Outflow. }
\end{array}\right.
$$

## Multiphase MOR : Numerical solution

## Iterative relaxation of the solid rotation constraint ${ }^{3}$

## At each time-step

Initial values $\boldsymbol{u}^{0}, p^{0}$ (e.g. from the previous time-step).
Initialize $\ell \leftarrow 0, \boldsymbol{\lambda}^{\ell} \leftarrow \mathbf{0}$
While not converge, do
Update $\ell \leftarrow \ell+1$
Solve for $\boldsymbol{u}^{\ell}, p^{\ell}$ :

$$
\begin{aligned}
& \rho\left(\delta_{t} \boldsymbol{u}^{\ell}+\nabla \boldsymbol{u}^{\ell} \cdot \mathbf{u}^{\ell} \mid \boldsymbol{v}\right)-\left(\boldsymbol{f}-\chi_{\mathrm{S}} \boldsymbol{\lambda}^{\ell-1} \mid \boldsymbol{v}\right)-\left(p^{\ell} \mid \nabla \cdot \boldsymbol{v}\right)+2 \eta\left(\mathrm{D}\left(\boldsymbol{u}^{\ell}\right) \mid \mathrm{D}(\boldsymbol{v})\right)=0, \\
& \left(\nabla \cdot \boldsymbol{u}^{\ell} \mid q\right)=0
\end{aligned}
$$

Uzawa update $\boldsymbol{\lambda}^{\ell}$ :
$\boldsymbol{\lambda}^{\ell} \leftarrow \boldsymbol{\lambda}^{\ell-1}+\boldsymbol{r}_{\mathrm{s}}\left(\boldsymbol{u}^{\ell}-\boldsymbol{u}_{\omega}\right)$
In the sequel, $v$ will be chosen as the POD modes.
3. Glowinski et Le Tallec, Augmented Lagrangian and operator-splitting methods in nonlinear mechanics, 1989.

## Standard ROM : POD of the fluctuating velocity

## Ersatz

$$
\widehat{\boldsymbol{u}}_{h}\left(\boldsymbol{x}, t_{n}\right)=\overline{\boldsymbol{u}}_{h}(\boldsymbol{x})+\sum_{i=1}^{n_{u}} \boldsymbol{\phi}_{i}^{\boldsymbol{u}}(\boldsymbol{x}) a_{i}\left(t_{n}\right)
$$

with

- $\overline{\boldsymbol{u}}_{h}(\boldsymbol{x})$ the time averaged velocity,
- $\boldsymbol{\Phi}^{u}=\left(\phi_{i}^{u}(x)\right)_{1 \leq i \leq n_{u}}$ the truncated POD basis,
- $\boldsymbol{a}=\left(a_{i}(t)\right)_{1 \leq i \leq n_{u}}$ the temporal coefficients.


## Remarks

- The velocity POD modes are divergence free $\nabla \cdot \phi_{i}^{u}=0,1 \leq i \leq n_{u}$ and the approximation $\widehat{\boldsymbol{u}}_{h}$ automatically satisfies the continuity equation $\nabla \cdot \widehat{\boldsymbol{u}}_{h}=0$.
- Dirichlet boundary conditions are all included in the mean field $\overline{\boldsymbol{u}}(\boldsymbol{x}) \Rightarrow$ POD modes vanish.


## ROM1 : Galerkin projection of the momentum equations

## Momentum equations

$$
\begin{equation*}
\mathbf{A} \cdot \frac{\mathrm{d} \boldsymbol{a}}{\mathrm{~d} t}+\mathbf{B} \cdot \boldsymbol{a}+\mathbf{C}: \boldsymbol{a} \otimes \boldsymbol{a}+\mathbf{E}^{\ell}+\mathbf{F}=\mathbf{0} \tag{3}
\end{equation*}
$$

## Uzawa update

$$
\begin{equation*}
\boldsymbol{\lambda}^{\ell+1}=\boldsymbol{\lambda}^{\ell}+r \chi_{\mathrm{S}}\left(\overline{\boldsymbol{u}}+\sum_{i=1}^{n_{u}} \phi_{i}^{\boldsymbol{u}} a_{i}-\boldsymbol{u}_{\omega}\right), \tag{4}
\end{equation*}
$$

Coefficients

$$
\left\{\begin{align*}
A_{i j} & =\rho\left(\phi_{j}^{u} \mid \phi_{i}^{u}\right)\left(=\rho \delta_{i j}\right),  \tag{5}\\
B_{i j} & =\rho\left(\nabla \phi_{j}^{u} \cdot \bar{u}+\nabla \bar{u} \cdot \phi_{j}^{u} \mid \phi_{i}^{u}\right)+2 \eta\left(\mathrm{D}\left(\phi_{j}^{u}\right) \mid \mathrm{D}\left(\phi_{i}^{u}\right)\right), \\
C_{i j k} & =\rho\left(\nabla \phi_{j}^{u} \cdot \phi_{k}^{u} \mid \phi_{i}^{u}\right), \\
E_{i}^{\ell} & =\left(\chi_{\mathrm{s}} \boldsymbol{\lambda}^{\ell} \mid \phi_{i}^{u}\right), \\
F_{i} & =\rho\left(\nabla \bar{u} \cdot \bar{u} \mid \phi_{i}^{u}\right)+2 \eta\left(\mathrm{D}\left(\phi_{j}^{u}\right) \mid \mathrm{D}\left(\phi_{i}^{u}\right)\right)-\left(\boldsymbol{f} \mid \phi_{i}^{u}\right) .
\end{align*}\right.
$$

Still depends on the high dimension due to projections !

## Proposed ROM : POD of the characteristic function

## Ersatz

$$
\widehat{\chi \mathrm{S}}(\boldsymbol{x}, t)=\overline{\chi \mathrm{s}}+\sum_{i=1}^{n_{\chi}} \phi_{i}^{\chi}(\boldsymbol{x}) c_{i}(\theta) .
$$

with

- $\overline{\chi_{\mathrm{s}}}(x)$ the angle averaged characteristic function,
- $\phi^{\chi}=\left(\phi_{i}^{\chi}(x)\right)_{1 \leq i \leq n_{\chi}}$ the truncated POD basis,
- $\boldsymbol{c}=\left(c_{i}(\theta)\right)_{1 \leq i \leq n_{\chi}}$ the angular coefficients.


## Remarks

- Forced rotation of the solid domain $\Rightarrow$ the $\theta: t \mapsto \theta(t)$ is known explicitly.
- The $\left(c_{i}(\theta)\right)_{1 \leq i \leq n_{\chi}}$ can be learned a priori (we use periodic splines).


## ROM2 : Galerkin projection of the Uzawa iteration

Now, due to the iterative procedure for updating the Lagrange multiplier $\boldsymbol{\lambda}$, the reduced Lagrange multiplier $\widehat{\boldsymbol{\lambda}}^{\ell}=\left(\widehat{\lambda}_{i}^{\ell}\right)_{1 \leq i \leq n_{u}}$ can be used in place of $\mathbf{E}^{\ell}$ in the reduced momentum equation (3) :

## Momentum equations

$$
\mathbf{A} \cdot \frac{\mathrm{d} \boldsymbol{a}}{\mathrm{~d} t}+\mathbf{B} \cdot \boldsymbol{a}+\mathbf{C}: \boldsymbol{a} \otimes \boldsymbol{a}+\hat{\lambda}^{\ell}+\mathbf{F}=\mathbf{0}
$$

Uzawa update

$$
\hat{\lambda}^{\ell+1}=\hat{\lambda}^{\ell}+r(\mathbf{G} \cdot \boldsymbol{a}+\mathbf{H} \cdot c+\mathbf{L}: c \otimes a+\mathbf{M})
$$

## Coefficients

$$
\left\{\begin{aligned}
\widehat{\lambda}_{i}^{\ell} & =\left(\chi_{\mathrm{s}} \lambda^{\ell} \mid \phi_{i}^{u}\right), \\
G_{i j} & =\left(\overline{\chi_{\mathrm{s}}} \phi_{j}^{u} \mid \phi_{i}^{u}\right), \\
H_{i k} & =\left(\phi_{k}^{\chi}\left(\overline{\boldsymbol{u}}-\boldsymbol{u}_{\omega}\right) \mid \phi_{i}^{u}\right), \\
L_{i j k} & =\left(\phi_{k}^{\chi} \phi_{j}^{u} \mid \phi_{i}^{u}\right) \\
M_{i} & =\left(\overline{\chi_{\mathrm{s}}}\left(\overline{\boldsymbol{u}}-\boldsymbol{u}_{\omega}\right) \mid \phi_{i}^{u}\right)
\end{aligned}\right.
$$

Does not depend on the high dimension!

## Interpolation of the reduced order models

## Question

Provided a set of POD bases $\left(\Phi\left(\lambda_{i}\right)\right)_{1 \leq i \leq N}$ with ${ }^{t} \Phi\left(\lambda_{i}\right) \Phi\left(\lambda_{i}\right)=\mathrm{I}_{m}$, how to derive the POD basis for a new parameter $\lambda$ without computing the full order solution ?

## One solution

Interpolate the set $\left(\Phi\left(\lambda_{i}\right)\right)_{1 \leq i \leq N}$ w.r.t the $\left(\lambda_{i}\right)_{1 \leq i \leq N}$
ROM1 : Interpolate POD basis for the velocity $\boldsymbol{\Phi}^{\boldsymbol{u}}$ only,
ROM2 : Interpolate POD bases for the velocity $\Phi^{\boldsymbol{u}}$ and the characteristic function $\Phi^{\chi}$ if the geometry changed

In this work, we focus on the interpolation over a set of Reynolds number (related with the solid rotation velocity), but the proposed method remains valid for multi-parameters setting.

## What are the proper objects to interpolate?

## POD-Galerkin ROM is independent of the choice of the POD basis

For every orthogonal matrix $A \in O(m)=\left\{B \in \mathbb{R}^{m \times m}:{ }^{T} B B=I_{m}\right\}$, we have

$$
\begin{aligned}
u_{\phi A} & =\Phi A^{T}(\phi A) u \\
& =\Phi\left(A^{T} A\right)^{T} \phi u \\
& =\Phi^{T} \Phi u \\
& =u_{\Phi}
\end{aligned}
$$

$\Rightarrow$ Interpolate the vectorial subspaces ${ }^{4}\left(\bar{\phi}_{i}\right)_{i=1}^{N}$ engendered by the POD bases $\left(\phi_{i}\right)_{i=1}^{N}$

- Interpolate in the set of all m-dimensional vectorial subspaces of the $n$-dimensional euclidian space.
- This is the the Grassmann manifold $G_{m}\left(\mathbb{R}^{n}\right)$, a differential manifold of dimension $m \times(n-m)$.

4. Amsallem et Farhat, "Interpolation method for adapting reduced-order models and application to aeroelasticity", 2008.

## Grassmannian Kriging

## Principle

1. Each point $\bar{\phi}_{i}$ is considered as the realization of a random process $Z=\mu+\delta$ with mean $\mu$ and $\delta$ a stationary random process with values in $T_{\bar{\phi}_{r}} G_{m}\left(\mathbb{R}^{n}\right)$ :

$$
Z_{i}=\exp _{\bar{\phi}_{r}}^{-1}\left(\bar{\phi}_{i}\right)
$$

2. Construct an experimental semivariogram from the data $\left(\bar{\phi}_{i}\right)_{i=1}^{N}$ and using the geodesic distance over $G_{m}\left(\mathbb{R}^{n}\right)$ (information on the spatial autocorrelation).
3. Depending on the spatial autocorrelation, we can choose an analytic semivariogram.
4. The weights $\left(\alpha_{i}(\lambda)\right)_{i=1}^{N}$ for the combination over a reference tangent space so that the variance is minimized are fully determined by the analytic semivariogram.

$$
Z^{\star}=\sum_{i=1}^{N} \alpha_{i}\left(\lambda^{\star}\right) Z_{i}
$$

5. Finally, combine the data in the tangent space at a reference point and get back on the Grassmann manifold

$$
\bar{\phi}^{\star}=\exp _{\bar{\Phi}_{r}}\left(Z^{\star}\right)
$$

## Compute the experimental semi-variogram (step 2)

The semi-variogram associated with $\delta$ is not known in practice.
An experimental semi-variogram is built from the data $\left(\bar{\Phi}_{i}\right)_{1 \leq i \leq n_{p}}$ as follows.
First, consider the following distances in the space of parameters

$$
\begin{align*}
m(\Lambda) & =\min \left\{\left\|\lambda_{i}-\lambda_{j}\right\|: 1 \leq i<j \leq N\right\}  \tag{6}\\
M(\Lambda) & =\max \left\{\left\|\lambda_{i}-\lambda_{j}\right\|: 1 \leq i<j \leq N\right\} \tag{7}
\end{align*}
$$

and $K \in \mathbb{N}$ such that $K \cdot m(\Lambda)<M(\Lambda)$.
Then ,define $h=\left(h_{0}, \cdots, h_{K+1}\right) \in \mathbb{R}^{K+2}$ where $h_{k}=k \cdot m(\Lambda)$ for all $k \in\{1, \cdots, K\}$, $h_{0}=0$ and $h_{K+1}=M(\Lambda)$.


## Algorithm to compute the experimental semi-variogram in step 2 (range and ceil)

```
compute \(m(\Lambda)=\min \left\{\left\|\lambda_{i}-\lambda_{j}\right\|: 1 \leq i<j \leq N\right\}\)
compute \(M(\Lambda)=\max \left\{\left\|\lambda_{i}-\lambda_{j}\right\|: 1 \leq i<j \leq N\right\}\)
    \(h_{0}=0\)
    for \(k=1\) to \(K+1\) do
    \(h_{k}=k \cdot m(\Lambda)\) if \(k<K+1\), else \(h_{k}=M(\Lambda)\)
    \(D_{k}=\emptyset \quad / /\) geodesic distances
    for \(i=1\) to \(N\) do
    for \(\underline{j=i+1}\) to \(N\) do
                if \(h_{k-1}<\left\|\lambda_{i}-\lambda_{j}\right\| \leq h_{k}\) then
                        Add \(\widehat{d}^{2}\left(\widehat{\log }\left(\Phi_{i}\right), \widehat{\log }\left(\Phi_{j}\right)\right)\) to the set \(D_{k} \quad / /\) geodesic \(d(\bullet)\)
                        end
            end
        end
        if \(\underline{\operatorname{Card}\left(D_{k}\right) \neq 0}\) then
            \(\widetilde{v}_{k}=\frac{1}{\operatorname{Card}\left(D_{k}\right)} \operatorname{Sum}\left(D_{k}\right)\)
        end
    end
\(18 a=h_{K+1} \quad / /\) Range
\(19 \quad c=\widetilde{v}_{K+1} \quad / /\) Ceil
```


## 2D Numerical experience : Rotating ellipse

Non-conforming mesh


## POD basis for the velocity



POD basis for the characteristic function


## Reconstruction of the characteristic function



## Overview

We choose $n_{\boldsymbol{u}}=30$ and $n_{\chi}=35$



Error $E(t)=\frac{\|\boldsymbol{u}(t)-\widehat{\boldsymbol{u}}(t)\|_{2}}{\|\boldsymbol{u}(t)\|_{2}}$
Time-saving
HDM $\simeq 7 \mathrm{~h}$,
ROM1 $\simeq 20 \mathrm{~min}$,
ROM2 $\simeq 1 \mathrm{~min}$.


## Numerical Results : Direct POD-ROMs

Fluctuating velocity

left : HDM

center: ROM1
right : ROM2


Vorticity


## Numerical Results : Direct POD-ROMs

Temporal coefficients for the velocity


Numerical Results : Interpolated POD-ROMs on transient period

Parameter is the Reynolds number. Sampling : $\operatorname{Re} \in(1000,1150,1350,1500)$. Interpolate at $\mathrm{Re}=1250$.


Numerical Results : Interpolated POD-ROMs on transient period

## Temporal coefficients for the velocity



## Conclusions

## Contributions

- Efficient procedure to build POD-ROM for flows induced by rigid rotating bodies.
- Introduction of the grassmannian krging interpolator.


## Perspectives

- Use of rotating frame for rotor subdomain $\Rightarrow$ Tearing-and-Coupling approach.
- Space/time Interpolations to avoid the resolution of the ROM.
- Extension of the proposed methods to tensor manifolds $\rightarrow$ PGD.
- Precise a priori estimation of interpolation errors.

Thank you for your attention.


[^0]:    1. Falaize, Liberge et Hamdouni, "POD-based reduced order model for flows induced by rigid solids in forced rotation", 2019.
    2. Mosquera, "Interpolation sur les variétés grassmanniennes et applications la réduction de modles en
